

Influence of mechanically activated hydrogen diffusivity on the toughness of metallic materials for the storage and transport of hydrogen under pressure

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Context

- Fully metallic (Type I) pressure vessels are limited by hydrogen embrittlement.
- The problem intensifies at high pressures, requiring new alloys and multilayer solutions, combining:
 - ❖ Low hydrogen permeability
 - ❖ High resistance to hydrogen embrittlement
 - ❖ Excellent mechanical strength
 - ❖ Cost-effectiveness to enable large-scale deployment

Type I (Fully Metallic)

Limiting pressure $P_{max} = 20-30$ MPa

Type IV (Fully Composite)

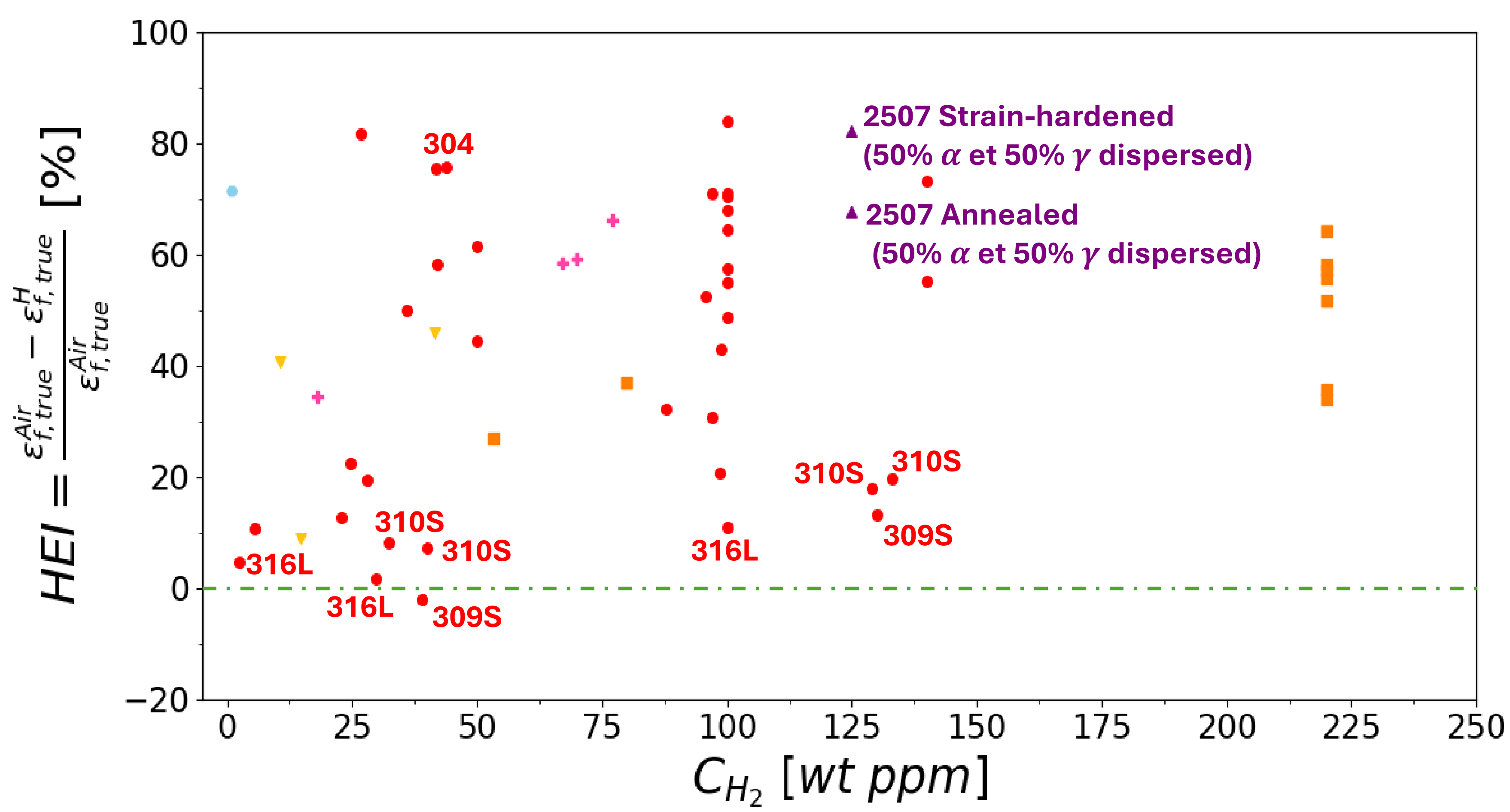
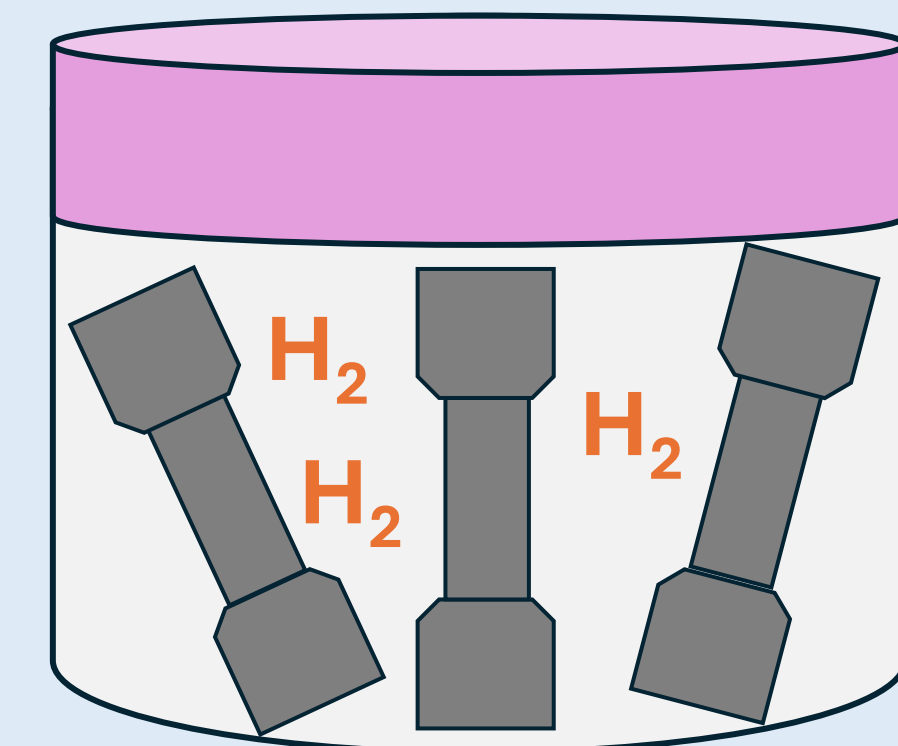
Limiting pressure $P_{max} = 70-80$ MPa

Goal: Reaching a storage pressure of 70MPa or more with cheaper fully metallic pressure vessels

Hydrogen embrittlement of steels

Hydrogen gaseous pre-charging and tensile testing in air

- Austenitic Stainless Steels
- High N Austenitic Stainless Steels
- ▼ Mn Austenitic Steels
- + Precipitation-Strengthened Austenitic Stainless Steels
- ▲ Duplex Stainless Steels
- Ferritic Stainless Steels



Higher susceptibility to hydrogen embrittlement

Austenitic stainless steels have the **highest resistance to hydrogen embrittlement** but:

- High amount of Ni: Expensive
- Low yield strength (200-320 MPa)

Need of new alloys

Materials with reduced or no Ni content and high yield strength: Dual-phase steels (Ferrite α /Austenite γ)

- ❖ Fe-Cr-Ni duplex stainless steels
- ❖ Fe-Mn dual phase steels

Improving hydrogen embrittlement resistance of dual-phase steels

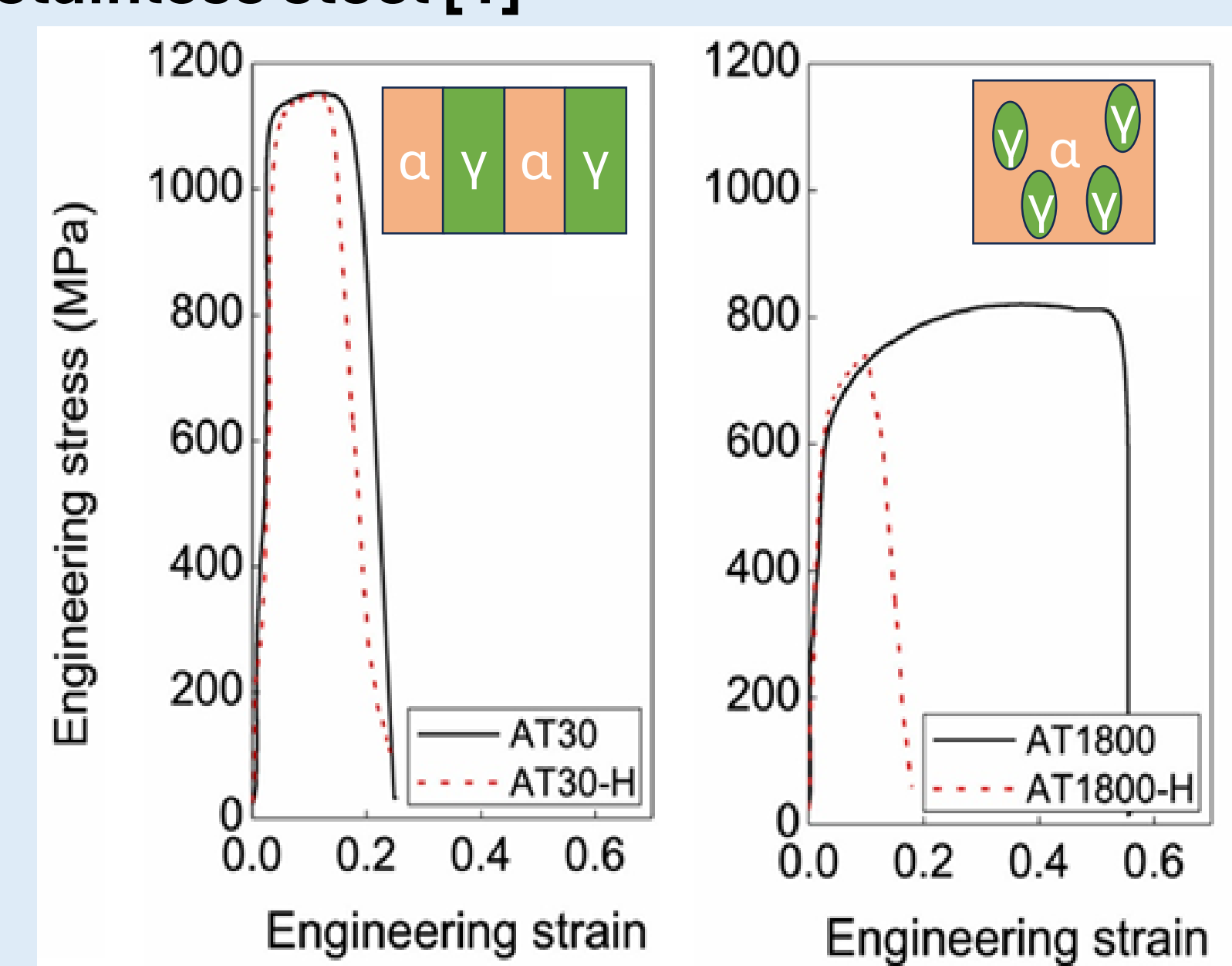
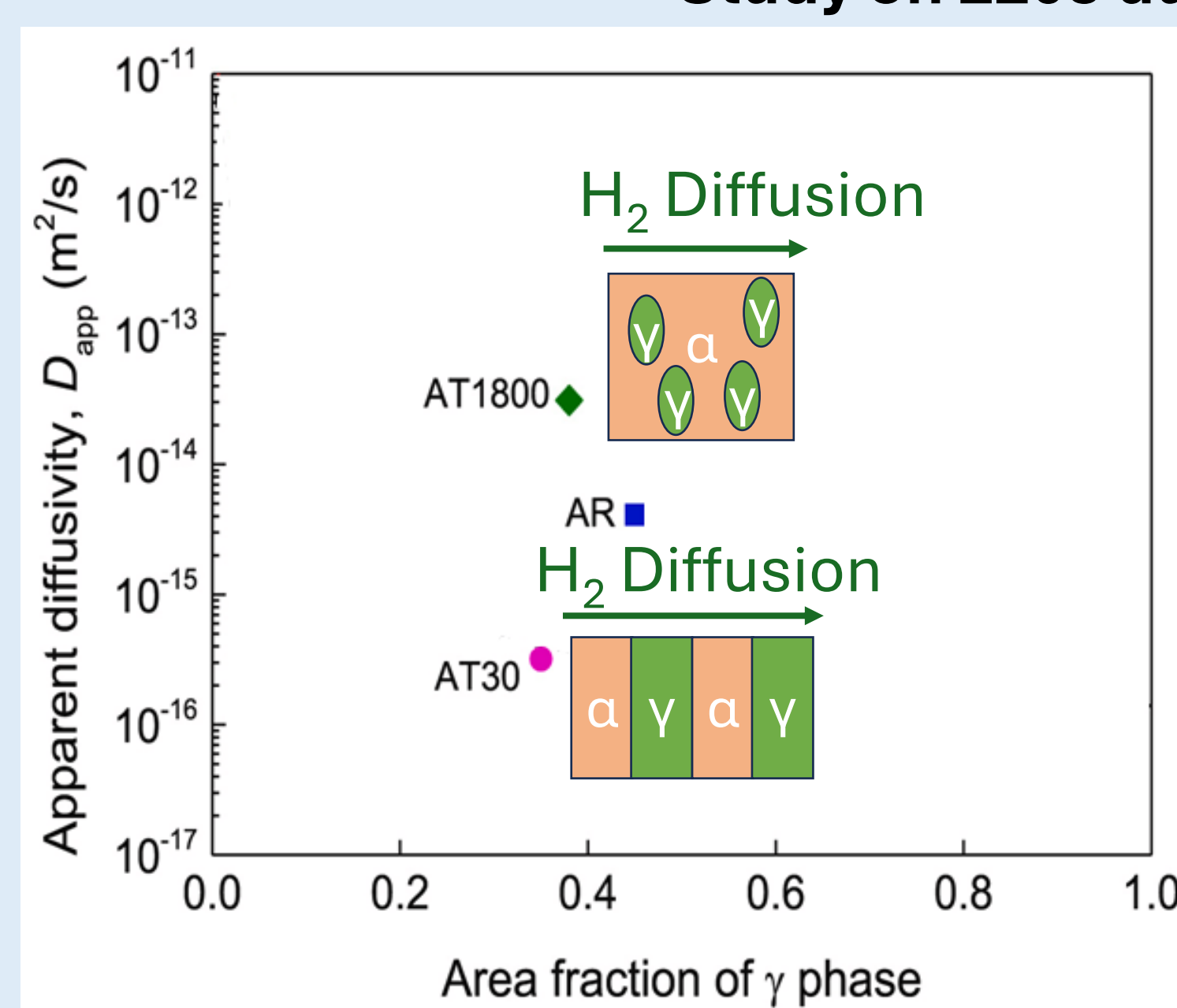
Study on 2205 duplex stainless steel [1]

Impact of:

- Austenite phase fraction
- Percolation of austenite
- Phase morphology

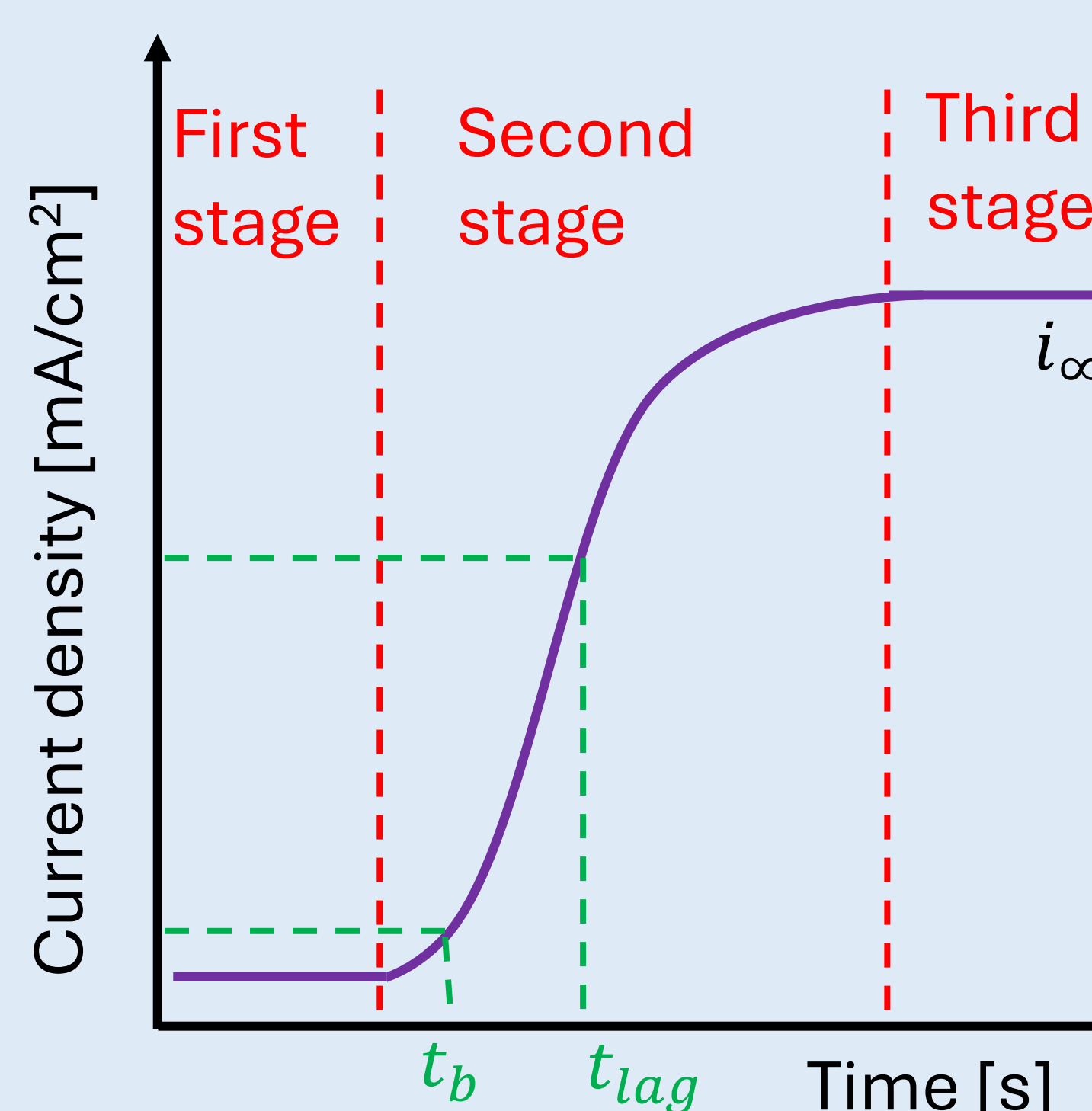
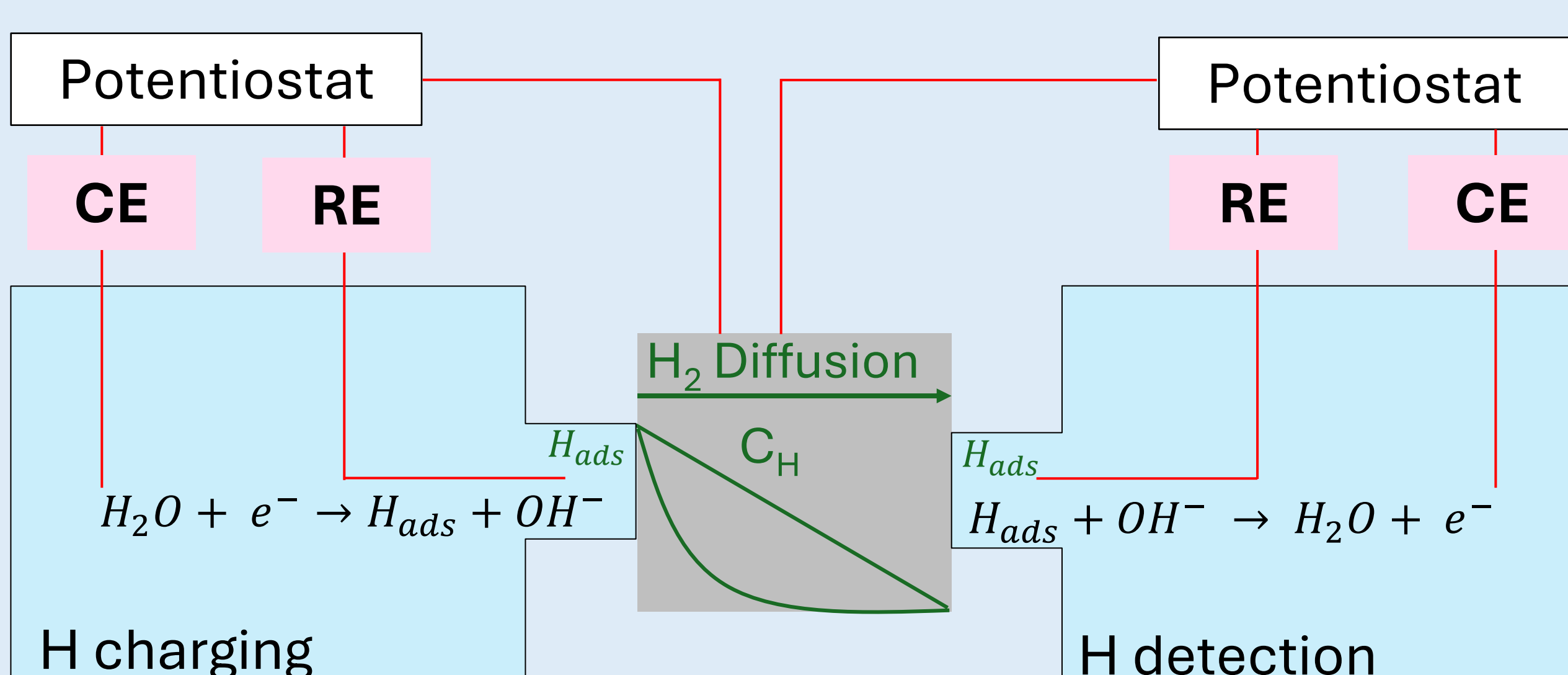
Studied through:

- Experimental work:
 - ❖ Electrochemical permeation
 - ❖ Gaseous permeation
 - ❖ Tensile testing after gaseous charging
- Numerical simulations using COMSOL



Electrochemical permeation

3-electrode cells:



Diffusivity measurements:

❖ Breakthrough time method:

$$D_{eff}(t_b) = \frac{L^2}{7.7 t_b}$$

❖ Time-lag method:

$$D_{eff}(t_{lag}) = \frac{L^2}{2 t_{lag}}$$

- ❖ Numerical methods

References

[1] Y. Wang et al., Influence of phase morphology on hydrogen embrittlement of type 2205 duplex stainless steel, <https://doi.org/10.1016/j.msea.2025.148335>

Acknowledgements

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